

ACCUMULATION QUANTIZATION

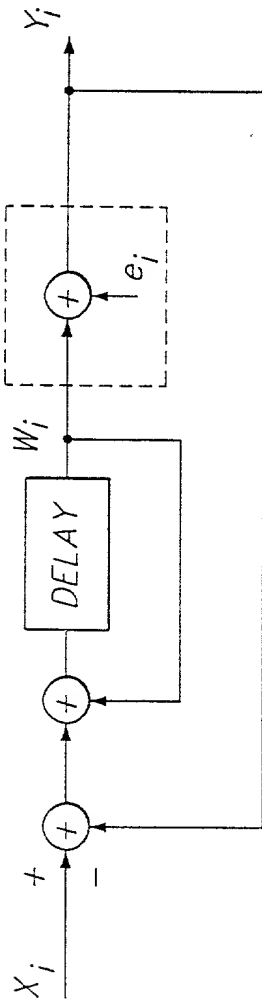


FIG. 1

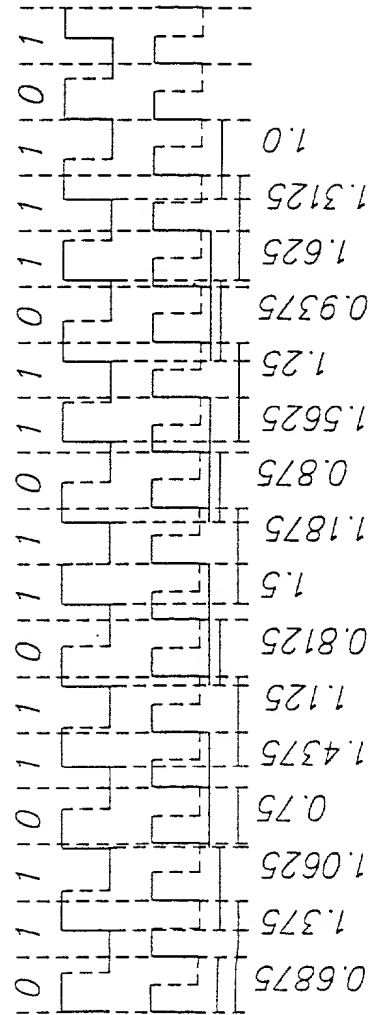


FIG. 3

Accumulator  
 $G_n = G_{n-1} + 0.6875 - INT(G_{n-1})$   
Data Stream  
 $R_n = INT(G_n)$

|        |   |
|--------|---|
| 0.6875 | 0 |
| 1.375  | 1 |
| 1.0625 | 1 |
| 0.75   | 0 |
| 1.4375 | 1 |
| 1.125  | 1 |
| 0.8125 | 0 |
| 1.5    | 1 |
| 1.1875 | 1 |
| 0.875  | 0 |
| 1.5625 | 1 |
| 1.25   | 1 |
| 0.9375 | 0 |
| 1.625  | 1 |
| 1.3125 | 1 |
| 1      | 1 |
| 0.6875 | 0 |

FIG. 2

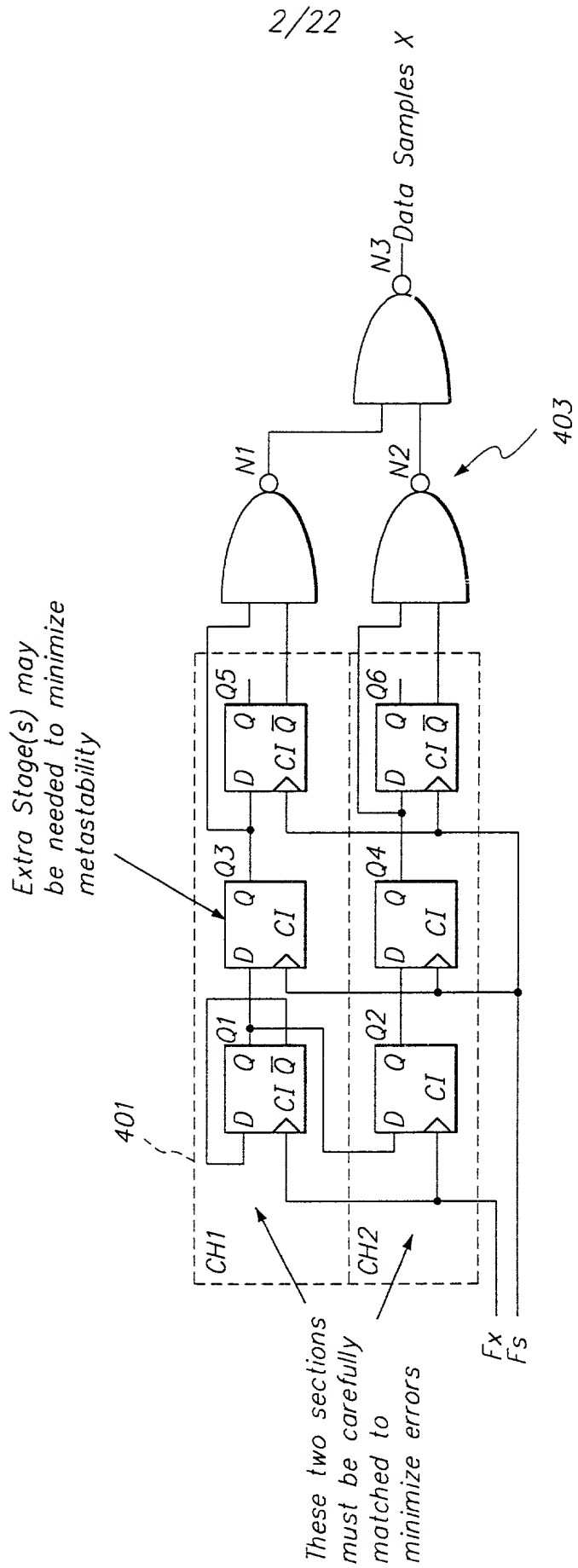


Fig. 4

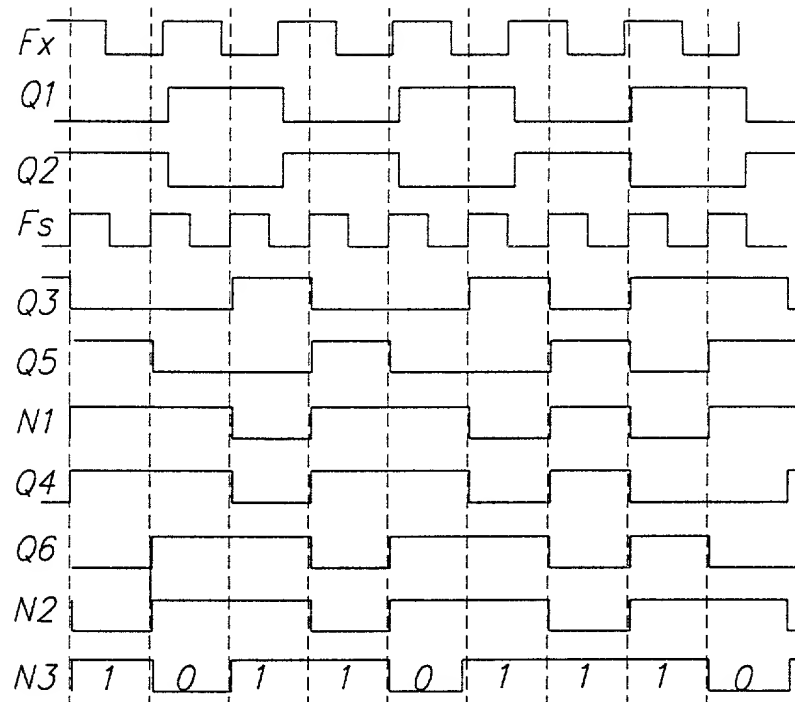


FIG. 5

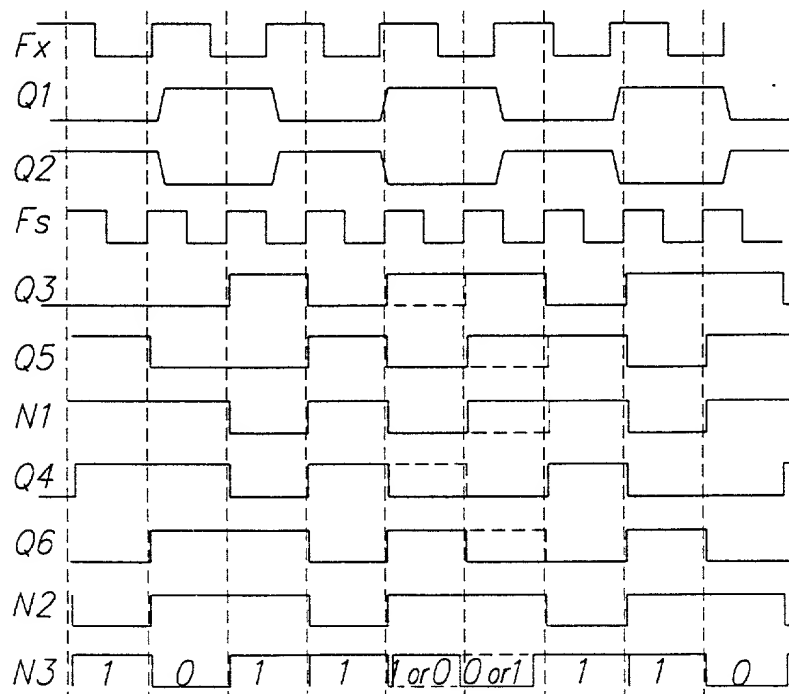


FIG. 6

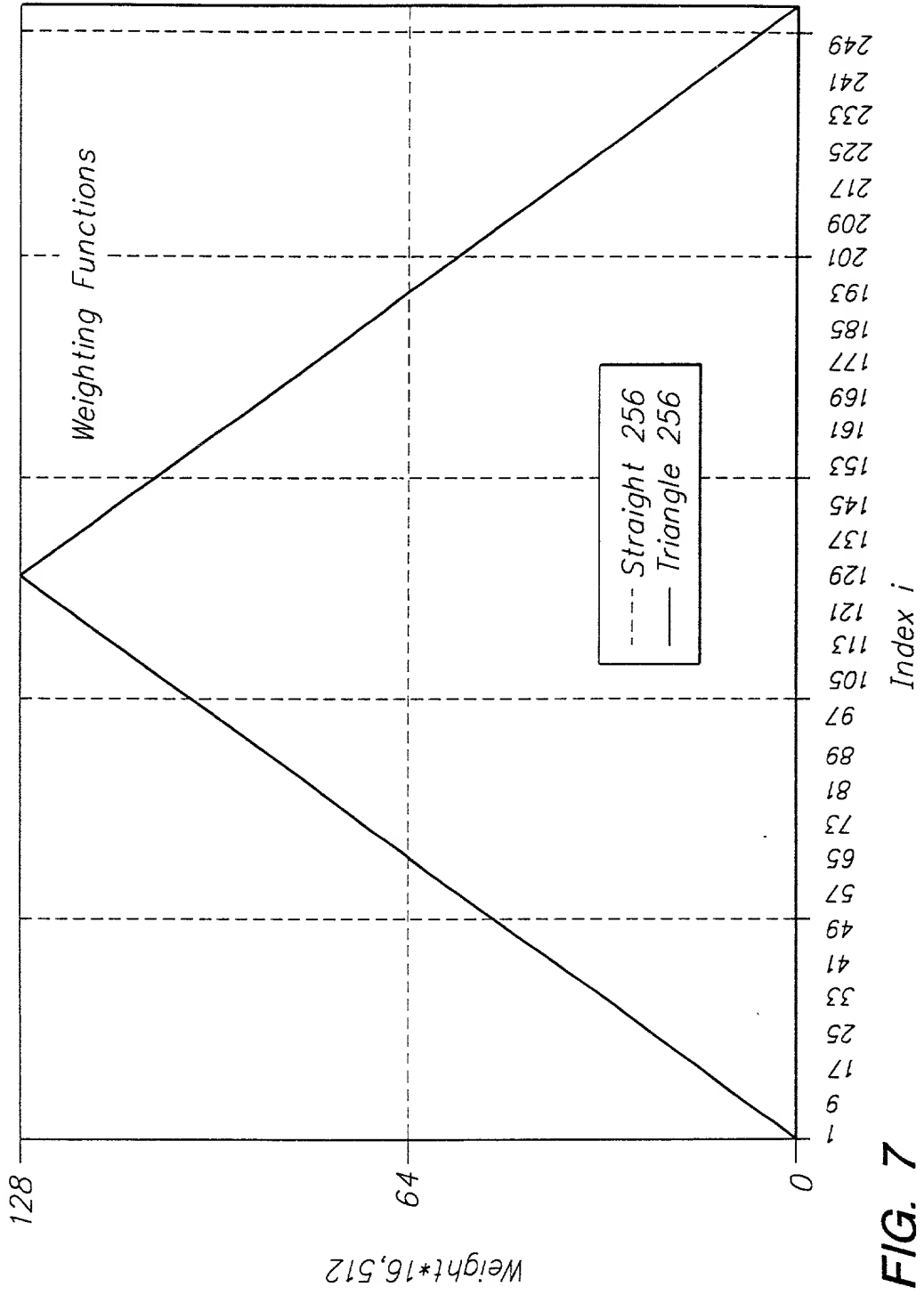


FIG. 7

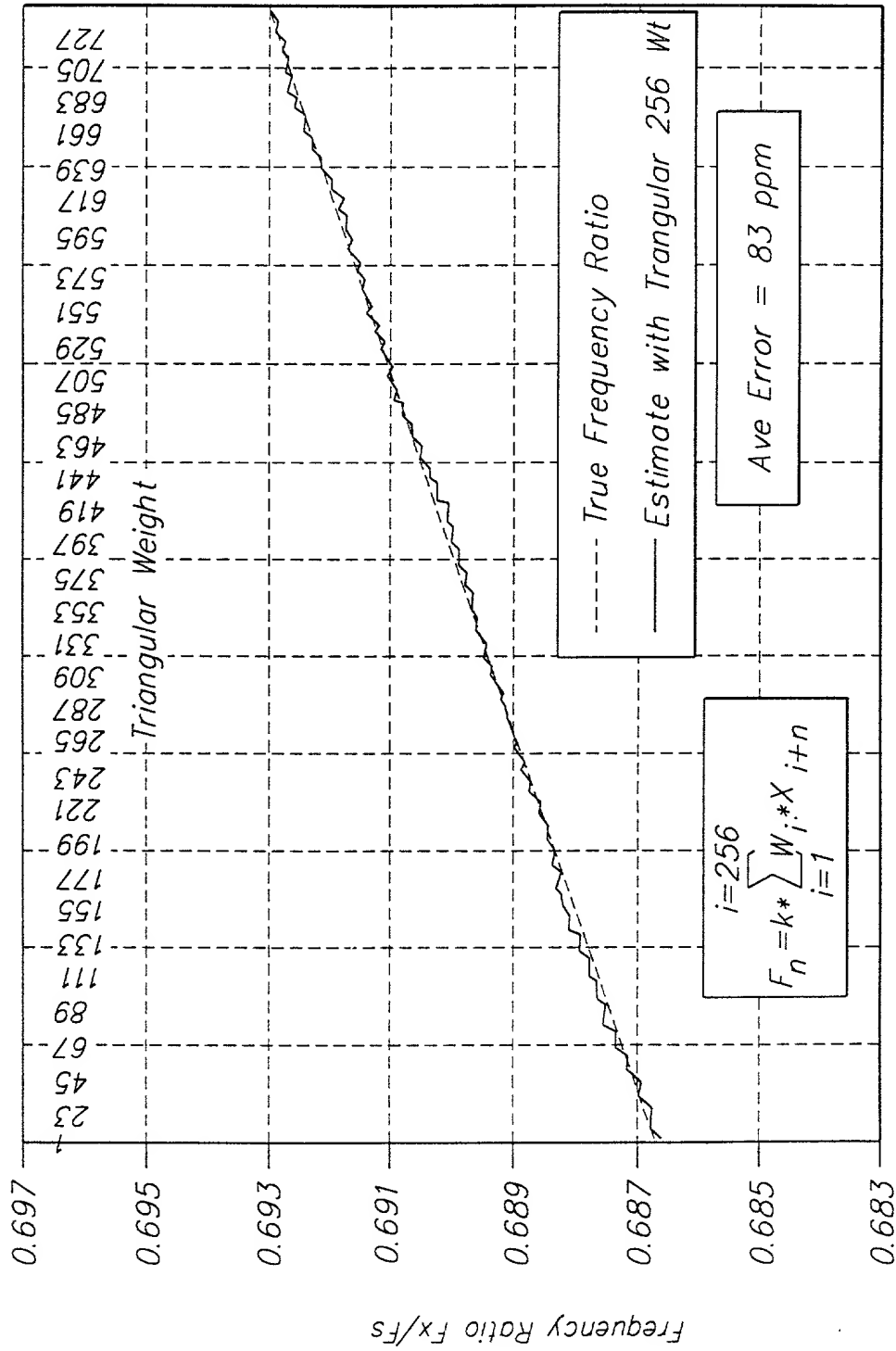


FIG. 9

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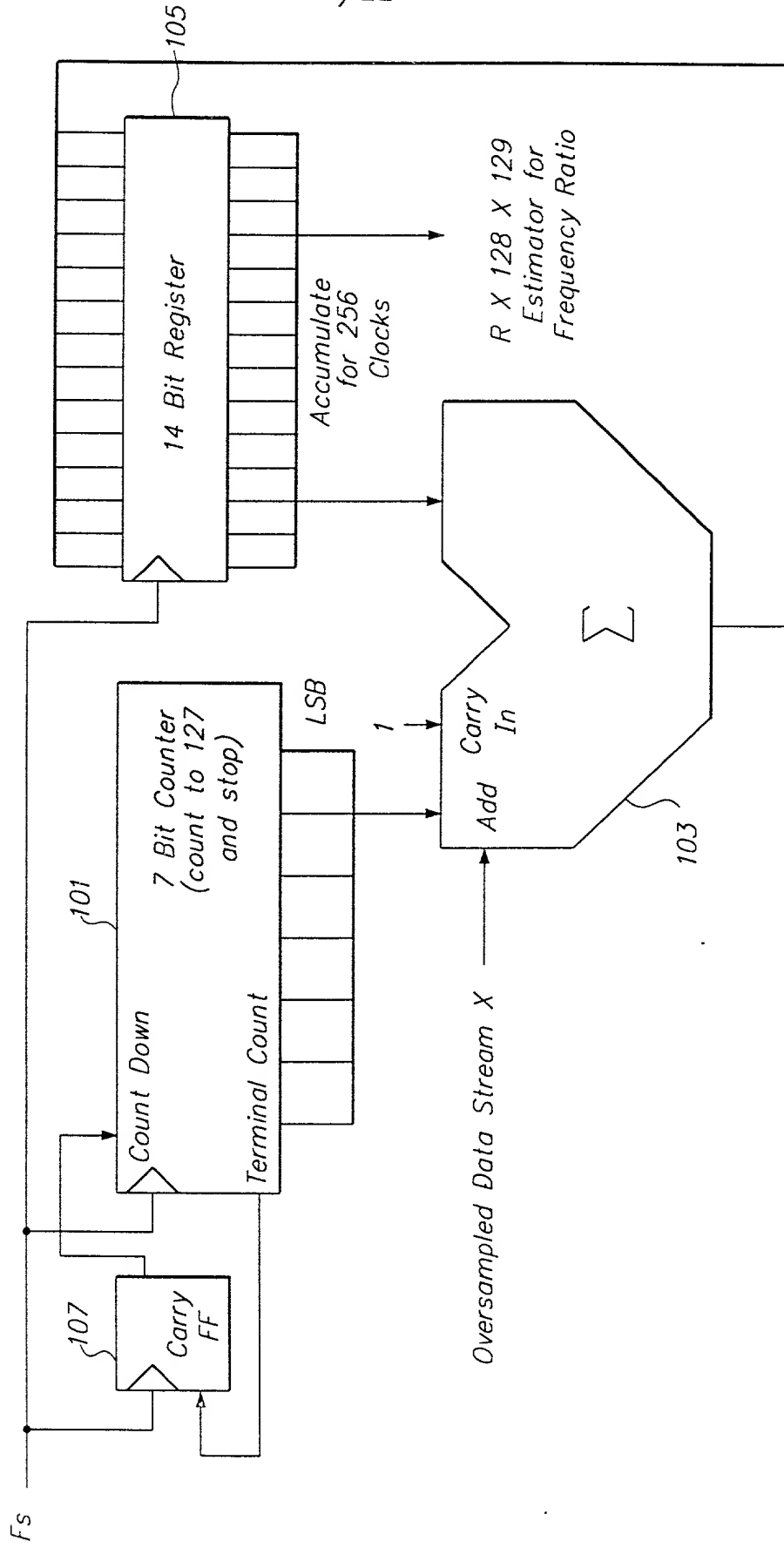


FIG. 10

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| Observed<br>Frequency<br>Data Stream<br><i>X</i> | Weight<br><i>W</i> | <i>Fr</i> Ratio =<br>Reference Frequency/<br>Sample Frequency = |
|--|--------------------|---|
| 1  | 1                  | 0.6875  |
| 1  | 2                  |   |
| 0  | 3                  |   |
| 1  | 4                  |   |
| 1  | 5                  |   |
| 0  | 6                  |   |
| 1  | 7                  |   |
| 1  | 8                  |   |
| 0  | 9                  |   |
| 1  | 10                 |   |
| 1  | 11                 |   |
| 1  | 12                 |   |
| 0  | 13                 |   |
| 1  | 14                 |   |
| 1  | 15                 |   |
| 0  | 16                 |   |
| 1  | 17                 |   |
| 1  | 18                 |   |
| 0  | 19                 |   |
| 1  | 20                 |   |
| 1  | 21                 |   |
| 0  | 22                 |   |
| 1  | 23                 |   |
| 1  | 24                 |   |
| 0  | 25                 |   |
| 1  | 26                 |   |
| 1  | 27                 |   |
| 1  | 28                 |   |
| 0  | 29                 |   |
| 1  | 30                 |   |
| 1  | 31                 |   |
| 0  | 32                 |   |
| 1  | 33                 |   |
| 1  | 34                 |   |
| 0  | 35                 |   |
| 1  | 36                 |   |
| 1  | 37                 |   |
| 0  | 38                 |   |
| 1  | 39                 |   |
| 1  | 40                 |   |
| 0  | 41                 |   |
| 1  | 42                 |   |
| 1  | 43                 |   |

**FIG. 11A-1**

**FIG. 11A-1**

**FIG. 11A-2**

**FIG. 11A**

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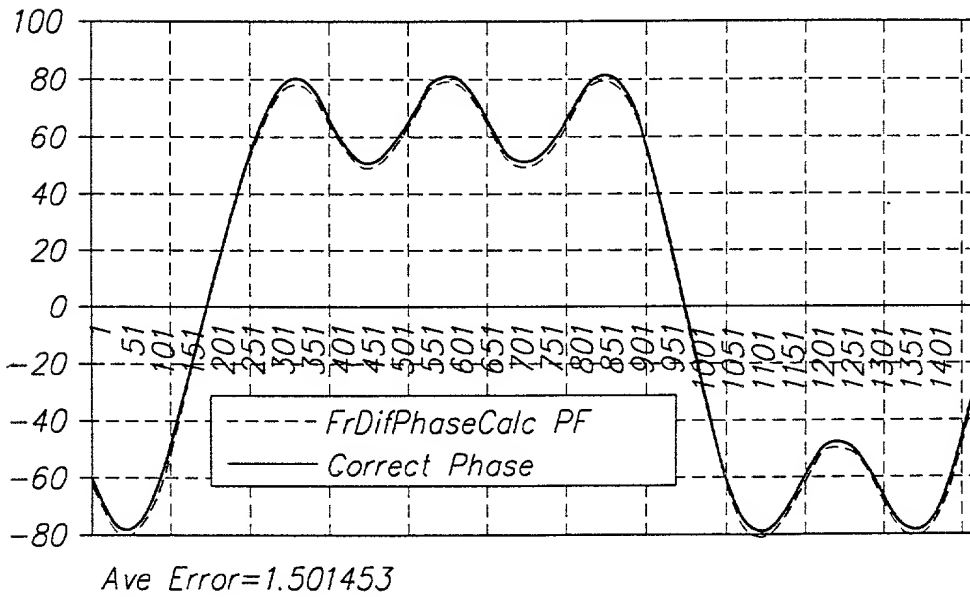
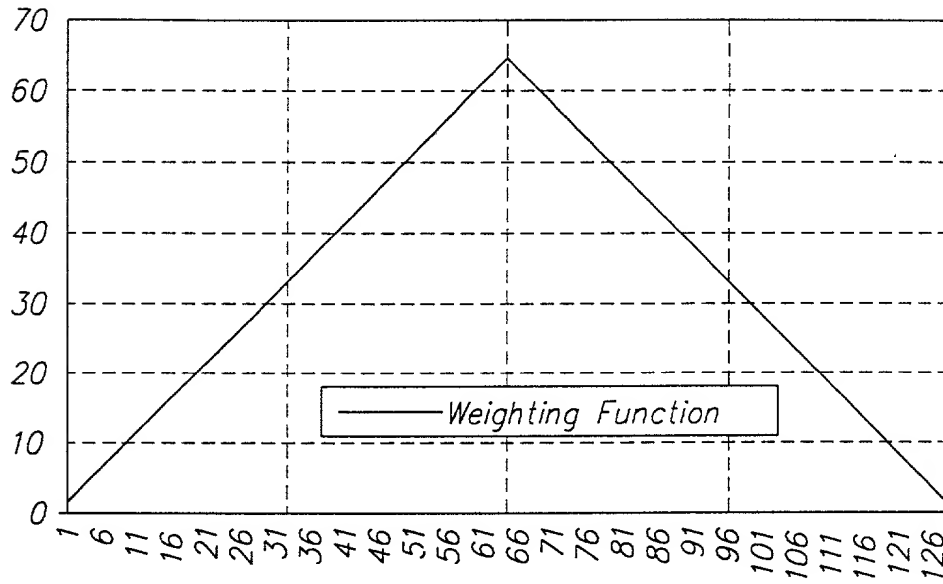
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| 0 | 44 |                    |  |   |   |
|---|----|--------------------|--|---|---|
| 1 | 45 |                    |  |   |   |
| 1 | 46 |                    |  |   |   |
| 1 | 47 |                    |  |   |   |
| 0 | 48 |                    |  |   |   |
| 1 | 49 |                    |  |   |   |
| 1 | 50 |                    |  |   |   |
| 0 | 51 |                    |  |   |   |
| 1 | 52 |                    |  |   |   |
| 1 | 53 |                    |  |   |   |
| 0 | 54 |                    |  |   |   |
| 1 | 55 |                    |  |   |   |
| 1 | 56 |                    |  |   |   |
| 0 | 57 |                    |  |   |   |
| 1 | 58 |                    |  |   |   |
| 1 | 59 |                    |  |   |   |
| 0 | 60 |                    |  |   |   |
| 1 | 61 |                    |  |   |   |
| 1 | 62 |                    |  |   |   |
| 1 | 63 |                    |  |   |   |
| 0 | 64 |                    |  |   |   |
|   |    | Frequency Estimate |  | Integration                                       |   |
|   |    | Correct<br>Phase   | $F_n =$<br>$\sum_i (W_i * X_{i+n})$<br>F | $\Delta F_i =$<br>$F_i - F_r$ Ratio<br>$\Delta F$ | $PF_n =$<br>$PF_{n-1} * k * \Delta F_i$<br>Pf |
| 1 | 64 | -53.714763         | 0.686058                                 | -0.001442   | -55.876923                                    |
| 1 | 63 | -54.394811         | 0.686058                                 | -0.001442   | -56.615385                                    |
| 0 | 62 | -55.066978         | 0.686058                                 | -0.001442   | -57.353846                                    |
| 1 | 61 | -55.731139         | 0.686058                                 | -0.001442   | -58.092308                                    |
| 1 | 60 | -56.387171         | 0.686058                                 | -0.001442   | -58.830769                                    |
| 0 | 59 | -57.034949         | 0.686058                                 | -0.001442   | -59.569231                                    |
| 1 | 58 | -57.674350         | 0.686058                                 | -0.001442   | -60.307692                                    |

FIG. 11A-2



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| Observed<br>Frequency<br>Data Stream<br>$X$ | Weight<br>$W$ | $Y_i = X_i - FrRatio$<br>$Y$ | $PX_i = PX_{i-1} + Y_i$<br>$P_x$ | $Fr Ratio =$<br>Reference Frequency/<br>Sample Frequency =<br>0.6875 |
|---|---------------|------------------------------|----------------------------------|--|
| 1   | 1             | 0.3125                       | 0.0000                           |  |
| 1   | 2             | 0.3125                       | 0.3125                           |  |
| 0   | 3             | -0.6875                      | -0.3750                          |  |
| 1   | 4             | 0.3125                       | -0.0625                          |  |
| 1   | 5             | 0.3125                       | 0.2500                           |  |
| 0   | 6             | -0.6875                      | -0.4375                          |  |
| 1   | 7             | 0.3125                       | -0.1250                          |  |
| 1   | 8             | 0.3125                       | 0.1875                           |  |
| 0   | 9             | -0.6875                      | -0.5000                          |  |
| 1   | 10            | 0.3125                       | -0.1875                          |  |
| 1   | 11            | 0.3125                       | 0.1250                           |  |
| 1   | 12            | 0.3125                       | 0.4375                           |  |
| 0   | 13            | -0.6875                      | -0.2500                          |  |
| 1   | 14            | 0.3125                       | 0.0625                           |  |
| 1   | 15            | 0.3125                       | 0.3750                           |  |
| 0   | 16            | -0.6875                      | -0.3125                          |  |
| 1   | 17            | 0.3125                       | 0.0000                           |  |
| 1   | 18            | 0.3125                       | 0.3125                           |  |
| 0   | 19            | -0.6875                      | -0.3750                          |  |
| 1   | 20            | 0.3125                       | -0.0625                          |  |
| 1   | 21            | 0.3125                       | 0.2500                           |  |
| 0   | 22            | -0.6875                      | -0.4375                          |  |
| 1   | 23            | 0.3125                       | -0.1250                          |  |
| 1   | 24            | 0.3125                       | 0.1875                           |  |
| 0   | 25            | -0.6875                      | -0.5000                          |  |
| 1   | 26            | 0.3125                       | -0.1875                          |  |
| 1   | 27            | 0.3125                       | 0.1250                           |  |
| 1   | 28            | 0.3125                       | 0.4375                           |  |
| 0   | 29            | -0.6875                      | -0.2500                          |  |
| 1   | 30            | 0.3125                       | 0.0625                           |  |
| 1   | 31            | 0.3125                       | 0.3750                           |  |
| 0   | 32            | -0.6875                      | -0.3125                          |  |
| 1   | 33            | 0.3125                       | 0.0000                           |  |
| 1   | 34            | 0.3125                       | 0.3125                           |  |
| 0   | 35            | -0.6875                      | -0.3750                          |  |
| 1   | 36            | 0.3125                       | -0.0625                          |  |
| 1   | 37            | 0.3125                       | 0.2500                           |  |
| 0   | 38            | -0.6875                      | -0.4375                          |  |
| 1   | 39            | 0.3125                       | -0.1250                          |  |
| 1   | 40            | 0.3125                       | 0.1875                           |  |
| 0   | 41            | -0.6875                      | -0.5000                          |  |
| 1   | 42            | 0.3125                       | -0.1875                          |  |
| 1   | 43            | 0.3125                       | 0.1250                           |  |

FIG. 12A-1

FIG. 12A-1

FIG. 12A-2

FIG. 12A

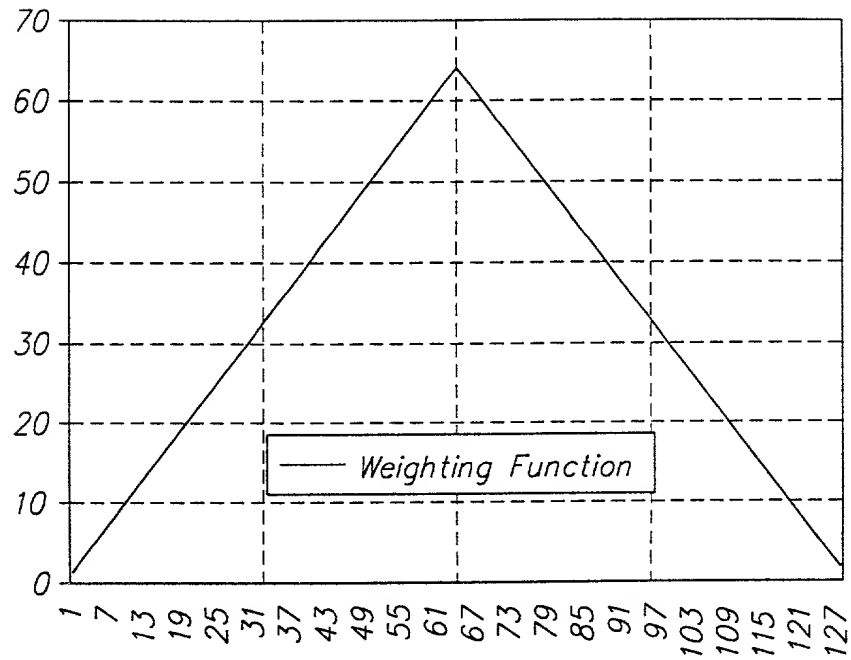
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|   |    |         |         |            |            |
|---|----|---------|---------|------------|------------|
| 0 | 44 | -0.6875 | -0.5625 |            |            |
| 1 | 45 | 0.3125  | -0.2500 |            |            |
| 1 | 46 | 0.3125  | 0.0625  |            |            |
| 1 | 47 | 0.3125  | 0.3750  |            |            |
| 0 | 48 | -0.6875 | -0.3125 |            |            |
| 1 | 49 | 0.3125  | 0.0000  |            |            |
| 1 | 50 | 0.3125  | 0.3125  |            |            |
| 0 | 51 | -0.6875 | -0.3750 |            |            |
| 1 | 52 | 0.3125  | -0.0625 |            |            |
| 1 | 53 | 0.3125  | 0.2500  |            |            |
| 0 | 54 | -0.6875 | -0.4375 |            |            |
| 1 | 55 | 0.3125  | -0.1250 |            |            |
| 1 | 56 | 0.3125  | 0.1875  |            |            |
| 0 | 57 | -0.6875 | -0.5000 |            |            |
| 1 | 58 | 0.3125  | -0.1875 |            |            |
| 1 | 59 | 0.3125  | 0.1250  |            |            |
| 0 | 60 | -0.6875 | -0.5625 |            |            |
| 1 | 61 | 0.3125  | -0.2500 |            |            |
| 1 | 62 | 0.3125  | 0.0625  |            |            |
| 1 | 63 | 0.3125  | 0.3750  |            |            |
| 0 | 64 | -0.6875 | -0.3125 |            |            |
| 1 | 64 | 0.3125  | 0.0000  | -53.714763 | -55.876923 |
| 1 | 63 | 0.3125  | 0.3125  | -54.394811 | -56.615385 |
| 0 | 62 | -0.6875 | -0.3750 | -55.066976 | -57.353846 |
| 1 | 61 | 0.3125  | -0.0625 | -55.731139 | -58.092308 |
| 1 | 60 | 0.3125  | 0.2500  | -56.387171 | -58.830769 |
| 0 | 59 | -0.6875 | -0.4376 | -57.034949 | -59.569231 |
| 1 | 58 | 0.3125  | -0.1250 | -57.674350 | -60.307692 |

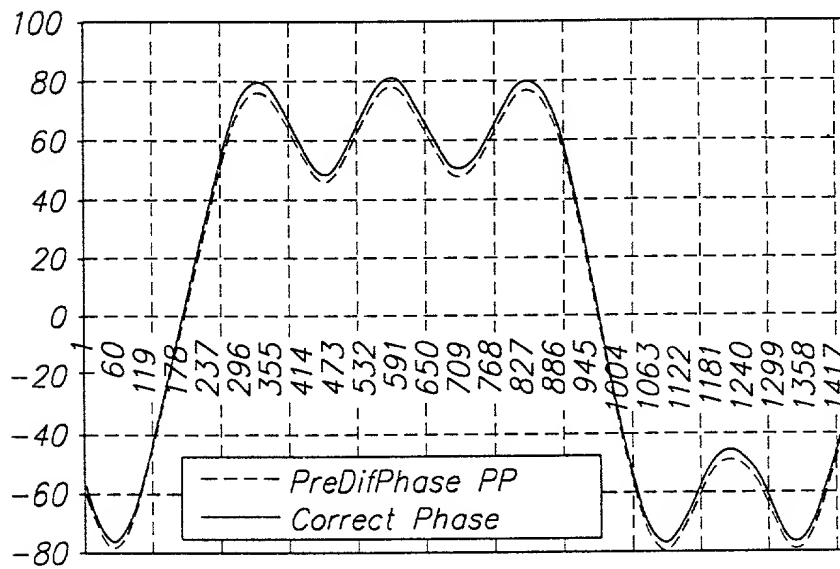
| Correct<br>Phase | $PP_n =$<br>$k \sum_i (W_i + PX_{i+n})$<br>PP |
|------------------|---|
|------------------|---|

FIG. 12A-2

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**FIG. 12B**



Ave Error= 1.501453

**FIG. 12C**

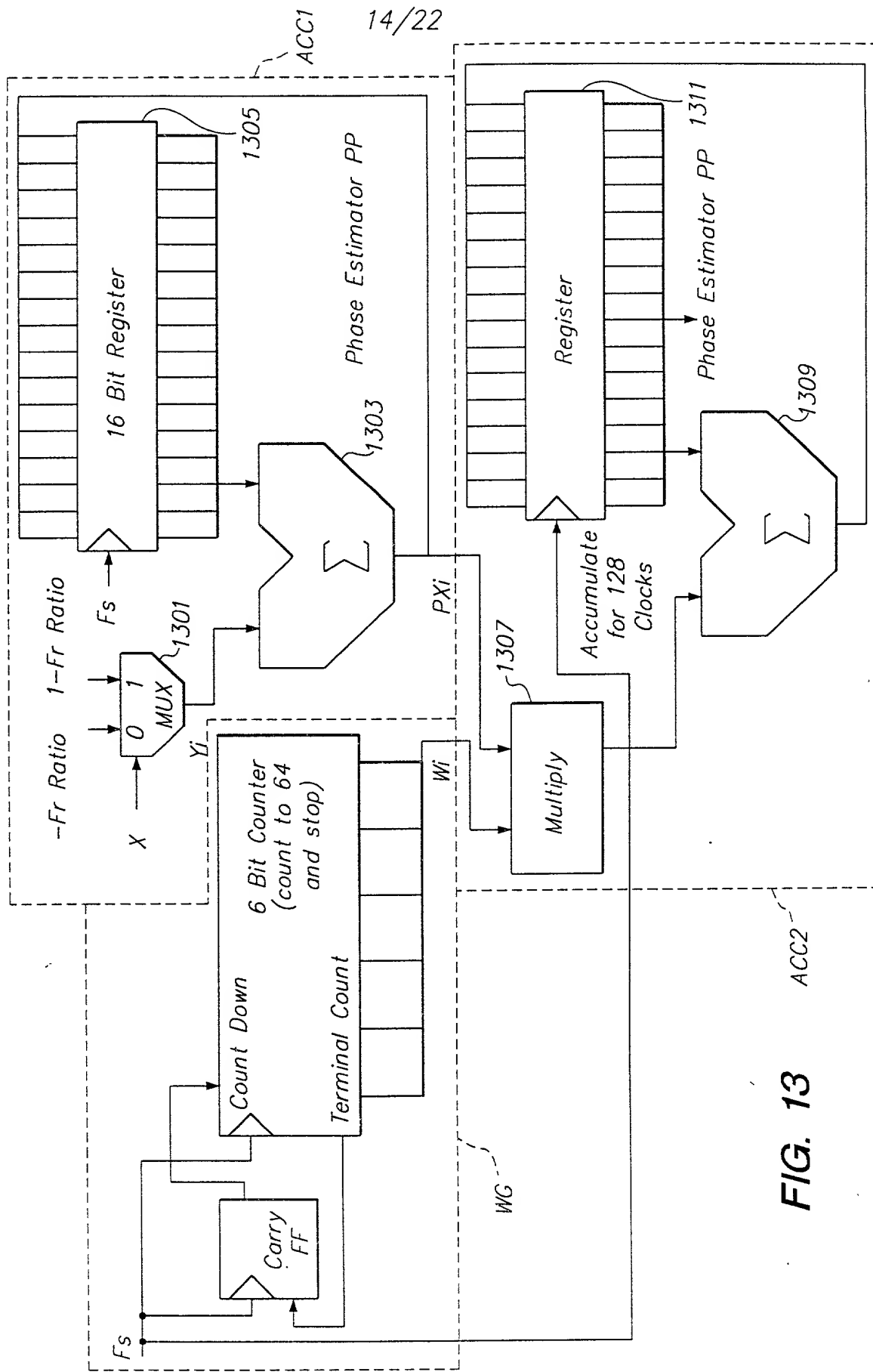


FIG. 13

| Reference<br>Frequency<br>Data Stream<br>$R$ | Observed<br>Frequency<br>Data System<br>$X$ | $D_i =$<br>$D_{i-1} + X_i - R_i$<br>$D$ | Weight<br>$W$ | Fr Ratio=<br>Reference Frequency/<br>Sample Frequency =<br>0.6875 |
|--|---|---|---------------|---|
| 1  | 1   | 0                                       | 1             |   |
| 1  | 1   | 0                                       | 2             |   |
| 0  | 0   | 0                                       | 3             |   |
| 1  | 1   | 0                                       | 4             |   |
| 1  | 1   | 0                                       | 5             |   |
| 0  | 0   | 0                                       | 6             |   |
| 1  | 1   | 0                                       | 7             |   |
| 1  | 1   | 0                                       | 8             |   |
| 1  | 0   | -1                                      | 9             |   |
| 0  | 1   | 0                                       | 10            |   |
| 1  | 1   | 0                                       | 11            |   |
| 1  | 1   | 0                                       | 12            |   |
| 0  | 0   | 0                                       | 13            |   |
| 1  | 1   | 0                                       | 14            |   |
| 1  | 1   | 0                                       | 15            |   |
| 0  | 0   | 0                                       | 16            |   |
| 1  | 1   | 0                                       | 17            |   |
| 1  | 1   | 0                                       | 18            |   |
| 0  | 0   | 0                                       | 19            |   |
| 1  | 1   | 0                                       | 20            |   |
| 1  | 1   | 0                                       | 21            |   |
| 0  | 0   | 0                                       | 22            |   |
| 1  | 1   | 0                                       | 23            |   |
| 1  | 1   | 0                                       | 24            |   |
| 1  | 0   | -1                                      | 25            |   |
| 0  | 1   | 0                                       | 26            |   |
| 1  | 1   | 0                                       | 27            |   |
| 1  | 1   | 0                                       | 28            |   |
| 0  | 0   | 0                                       | 29            |   |
| 1  | 1   | 0                                       | 30            |   |
| 1  | 1   | 0                                       | 31            |   |
| 0  | 0   | 0                                       | 32            |   |
| 1  | 1   | 0                                       | 33            |   |
| 1  | 1   | 0                                       | 34            |   |
| 0  | 0   | 0                                       | 35            |   |
| 1  | 1   | 0                                       | 36            |   |
| 1  | 1   | 0                                       | 37            |   |
| 0  | 0   | 0                                       | 38            |   |
| 1  | 1   | 0                                       | 39            |   |
| 1  | 1   | 0                                       | 40            |   |
| 1  | 0   | -1                                      | 41            |   |
| 0  | 1   | 0                                       | 42            |   |

**FIG. 14A-1****FIG. 14A-1****FIG. 14A-2****FIG. 14A**

|   |   |    |    |               |   |
|---|---|----|----|---------------|---|
| 1 | 1 | 0  | 43 |               |   |
| 1 | 0 | -1 | 44 |               |   |
| 0 | 1 | 0  | 45 |               |   |
| 1 | 1 | 0  | 46 |               |   |
| 1 | 1 | 0  | 47 |               |   |
| 0 | 0 | 0  | 48 |               |   |
| 1 | 1 | 0  | 49 |               |   |
| 1 | 1 | 0  | 50 |               |   |
| 0 | 0 | 0  | 51 |               |   |
| 1 | 1 | 0  | 52 |               |   |
| 1 | 1 | 0  | 53 |               |   |
| 0 | 0 | 0  | 54 |               |   |
| 1 | 1 | 0  | 55 |               |   |
| 1 | 1 | 0  | 56 |               |   |
| 1 | 0 | -1 | 57 |               |   |
| 0 | 1 | 0  | 58 |               |   |
| 1 | 1 | 0  | 59 |               |   |
| 1 | 0 | -1 | 60 |               |   |
| 0 | 1 | 0  | 61 |               |   |
| 1 | 1 | 0  | 62 |               |   |
| 1 | 1 | 0  | 63 |               |   |
| 0 | 0 | 0  | 64 |               |   |
| 1 | 1 | 0  | 64 | Correct Phase | $PI_n =$<br>$k_0 + k_1 * \sum_i (W_i * D_{i+n})$<br>$F$ |
| 1 | 1 | 0  | 63 | -53.714763    | -55.876923  |
| 0 | 0 | 0  | 62 | -54.394811    | -56.615385  |
| 1 | 1 | 0  | 61 | -55.066978    | -57.353846  |
| 1 | 1 | 0  | 60 | -55.731139    | -58.092308  |
| 1 | 1 | 0  | 60 | -56.387171    | -58.830769  |
| 0 | 0 | 0  | 59 | -57.034949    | -59.569231  |
| 1 | 1 | 0  | 58 | -57.674350    | -60.307692  |

 $k_0 = 16$ 

FIG. 14A-2

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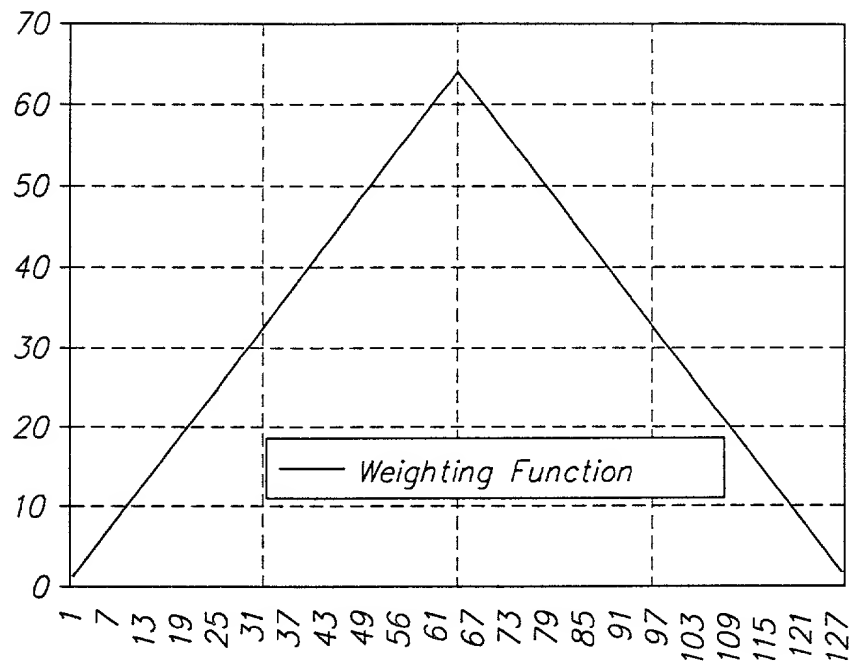
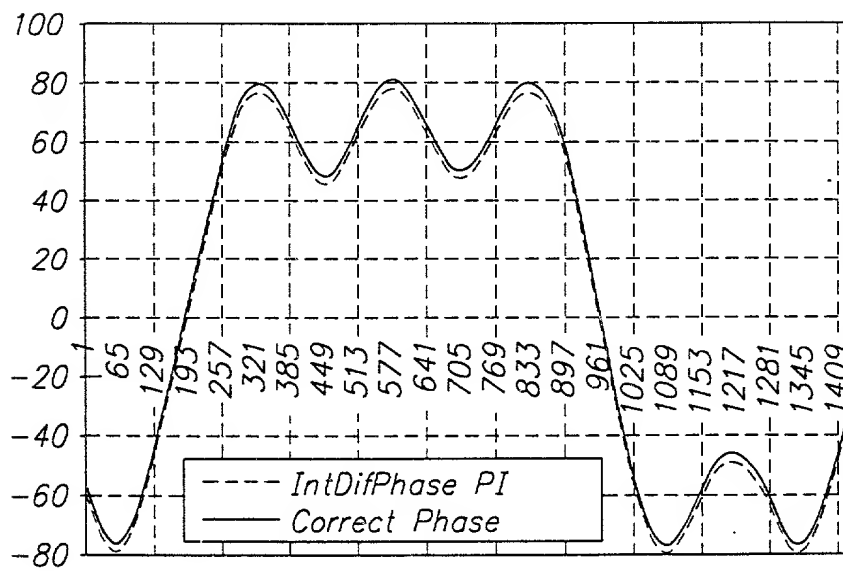


FIG. 14B



Ave Error= 1.501453

FIG. 14C



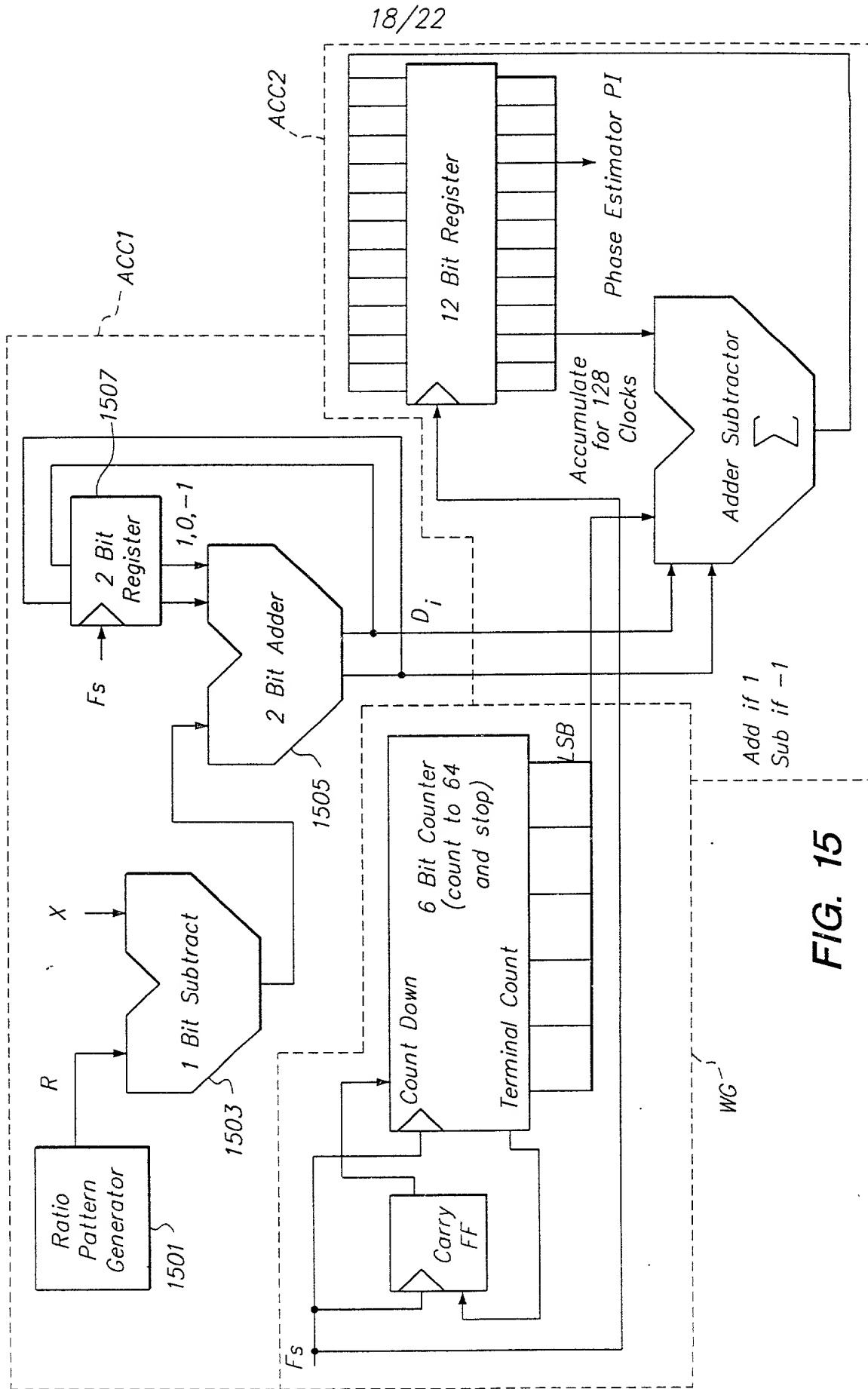


FIG. 15

| Reference<br>Frequency<br>Generator<br>RG | Reference<br>Frequency<br>Data Stream<br>R | Observed<br>Frequency<br>Data System<br>X | $D_i =$<br>$D_{i-1} + X_i - R_i$<br>D | Weight<br>W | Fr Ratio=<br>Reference Frequency/<br>Sample Frequency =<br>0.6875 |
|---|--|---|---------------------------------------|-------------|---|
| 1.5                                       | 1  | 1   | 0                                     | -0.5        |   |
| 1.1875                                    | 1  | 1   | 0                                     | -2          |   |
| 0.875                                     | 0  | 0   | 0                                     | -4.5        |   |
| 1.5625                                    | 1  | 1   | 0                                     | -8          |   |
| 1.25                                      | 1  | 1   | 0                                     | -12.5       |   |
| 0.9375                                    | 0  | 0   | 0                                     | -18         |   |
| 1.625                                     | 1  | 1   | 0                                     | -24.5       |   |
| 1.3125                                    | 1  | 1   | 0                                     | -32         |   |
| 1   | 1  | 0   | -1                                    | -40.5       |   |
| 0.6675                                    | 0  | 1   | 0                                     | -50         |   |
| 1.375                                     | 1  | 1   | 0                                     | -60.5       |   |
| 1.0625                                    | 1  | 1   | 0                                     | -72         |   |
| 0.75                                      | 0  | 0   | 0                                     | -84.5       |   |
| 1.4375                                    | 1  | 1   | 0                                     | -98         |   |
| 1.125                                     | 1  | 1   | 0                                     | -112.5      |   |
| 0.8125                                    | 0  | 0   | 0                                     | -128        |   |
| 1.5                                       | 1  | 1   | 0                                     | -144.5      |   |
| 1.1875                                    | 1  | 1   | 0                                     | -162        |   |
| 0.875                                     | 0  | 0   | 0                                     | -180.5      |   |
| 1.5625                                    | 1  | 1   | 0                                     | -200        |   |
| 1.25                                      | 1  | 1   | 0                                     | -220.5      |   |
| 0.9375                                    | 0  | 0   | 0                                     | -242        |   |
| 1.625                                     | 1  | 1   | 0                                     | -264.5      |   |
| 1.3125                                    | 1  | 1   | 0                                     | -288        |   |
| 1   | 1  | 0   | -1                                    | -312.5      |   |
| 0.6875                                    | 0  | 1   | 0                                     | -338        |   |
| 1.375                                     | 1  | 1   | 0                                     | -364.5      |   |
| 1.0625                                    | 1  | 1   | 0                                     | -392        |   |
| 0.75                                      | 0  | 0   | 0                                     | -420.5      |   |
| 1.4375                                    | 1  | 1   | 0                                     | -450        |   |
| 1.125                                     | 1  | 1   | 0                                     | -480.5      |   |
| 0.8125                                    | 0  | 0   | 0                                     | -512        |   |
| 1.5                                       | 1  | 1   | 0                                     | -644.5      |   |
| 1.1875                                    | 1  | 1   | 0                                     | -578        |   |
| 0.875                                     | 0  | 0   | 0                                     | -612.5      |   |
| 1.5625                                    | 1  | 1   | 0                                     | -648        |   |
| 1.25                                      | 1  | 1   | 0                                     | -684.5      |   |
| 0.9375                                    | 0  | 0   | 0                                     | -722        |   |
| 1.625                                     | 1  | 1   | 0                                     | -760.6      |   |
| 1.3125                                    | 1  | 1   | 0                                     | -800        |   |
| 1   | 1  | 0   | -1                                    | -840.5      |   |
| 0.6875                                    | 0  | 1   | 0                                     | 882         |   |

FIG.  
16A-1

FIG. 16A-2

FIG. 16A

FIG. 16A-1

| 1.375  | 1 | 1 | 0  | -924.5  |
|--------|---|---|----|---------|
| 1.0625 | 1 | 0 | -1 | -968    |
| 0.75   | 0 | 1 | 0  | -1012.5 |
| 1.4375 | 1 | 1 | 0  | -1068   |
| 1.125  | 1 | 1 | 0  | -1104.5 |
| 0.8125 | 0 | 0 | 0  | -1152   |
| 1.5    | 1 | 1 | 0  | -1200.5 |
| 1.1875 | 1 | 1 | 0  | -1250   |
| 0.875  | 0 | 0 | 0  | -1300.5 |
| 1.5625 | 1 | 1 | 0  | -1352   |
| 1.25   | 1 | 1 | 0  | -1404.5 |
| 0.9375 | 0 | 0 | 0  | -1458   |
| 1.625  | 1 | 1 | 0  | -1512.5 |
| 1.3125 | 1 | 1 | 0  | -1568   |
| 1      | 1 | 0 | -1 | -1624.5 |
| 0.6875 | 0 | 1 | 0  | -1682   |
| 1.375  | 1 | 1 | 0  | -1740.5 |
| 1.0625 | 1 | 0 | -1 | -1800   |
| 0.75   | 0 | 1 | 0  | -1860.5 |
| 1.4375 | 1 | 1 | 0  | -1922   |
| 1.125  | 1 | 1 | 0  | -1984.5 |
| 0.8125 | 0 | 0 | 0  | -2048   |
| 1.5    | 1 | 1 | 0  | 2048    |
| 1.1875 | 1 | 1 | 0  | 1984.5  |
| 0.875  | 0 | 0 | 0  | 1922    |
| 1.5625 | 1 | 1 | 0  | 1860.5  |
| 1.25   | 1 | 1 | 0  | 1800    |
| 0.9375 | 0 | 0 | 0  | 1740.5  |
| 1.625  | 1 | 1 | 0  | 1682    |
| 1.3125 | 1 | 1 | 0  | 1624.5  |

Correct Phase

$PC_n =$   
 $k*(D_n - \text{frac}(RG_n) + 0.5 + \sum_i (W_i * X_{i+n-64}))$   
PC

|            |            |
|------------|------------|
| -53.374738 | -55.507692 |
| -54.054787 | -56.246154 |
| -54.730895 | -56.984615 |
| -55.399059 | -57.723077 |
| -56.059155 | -58.461538 |
| -56.711060 | -59.200000 |
| -57.354650 | -59.938462 |
| -57.939800 | -60.676923 |

FIG. 16A-2

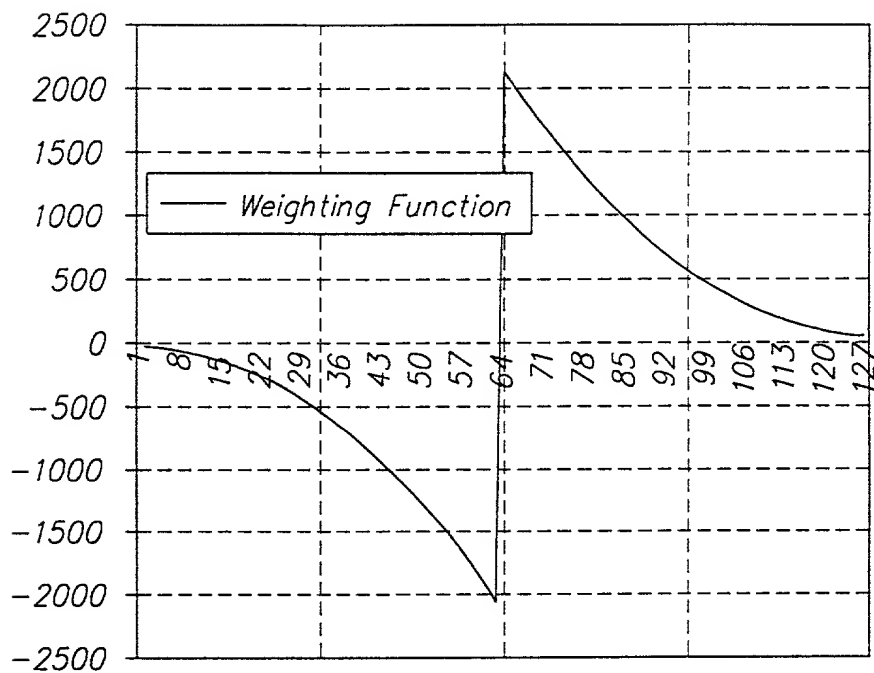
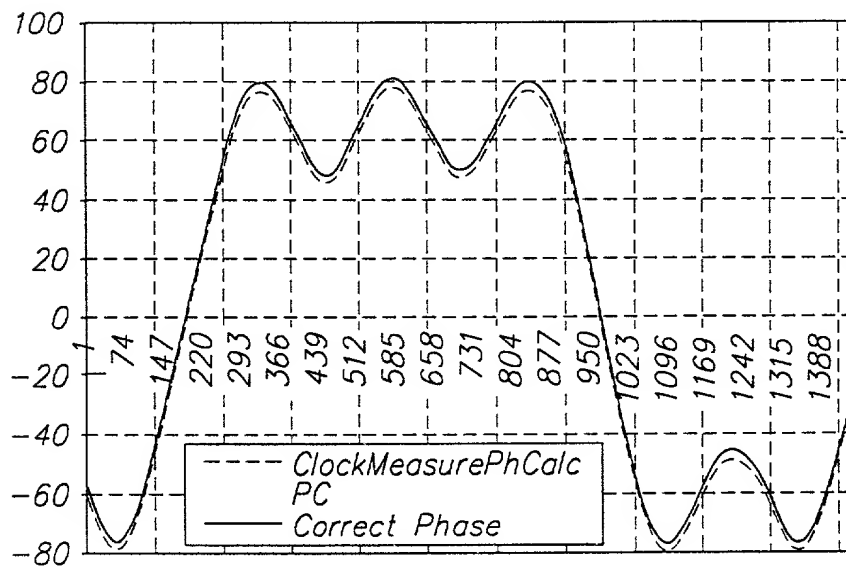


FIG. 16B



Ave Error= 1.501476

FIG. 16C

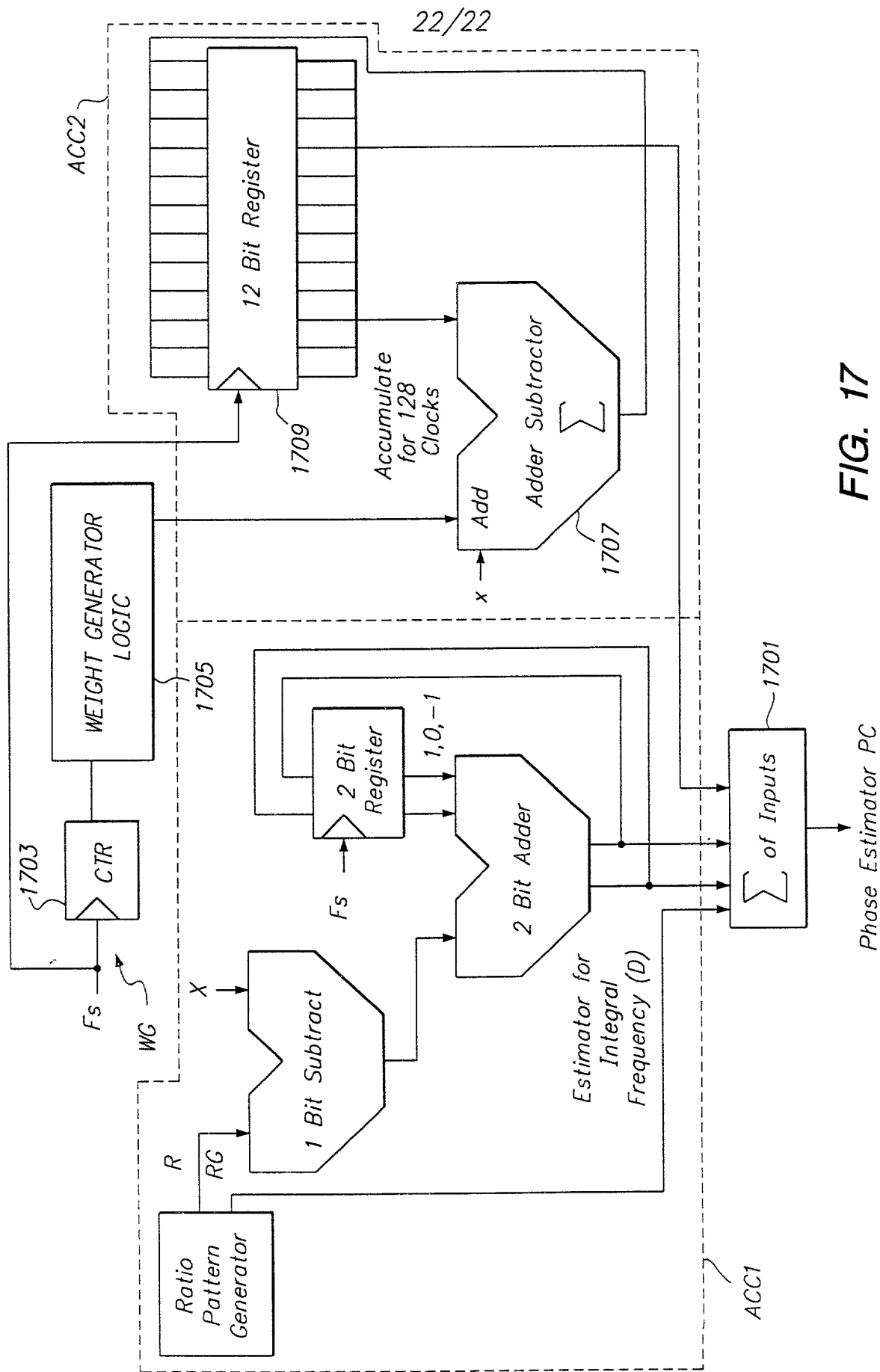


FIG. 17